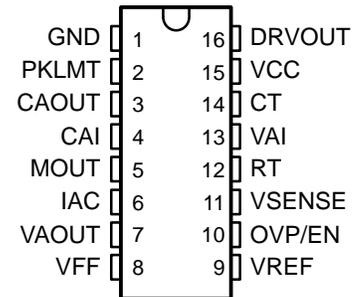


- Controls Boost Preregulator to Near-Unity Power Factor
- World Wide Line Operation
- Over-Voltage Protection
- Accurate Power Limiting
- Average Current Mode Control
- Improved Noise Immunity
- Improved Feed-Forward Line Regulation
- Leading Edge Modulation
- 150- μ A Typical Start-Up Current
- Low-Power BiCMOS Operation
- 10.8-V to 17-V Operation
- Programmable Output Voltage (Tracking Boost Topology)

D, DW, N, and PW PACKAGES
(TOP VIEW)



description

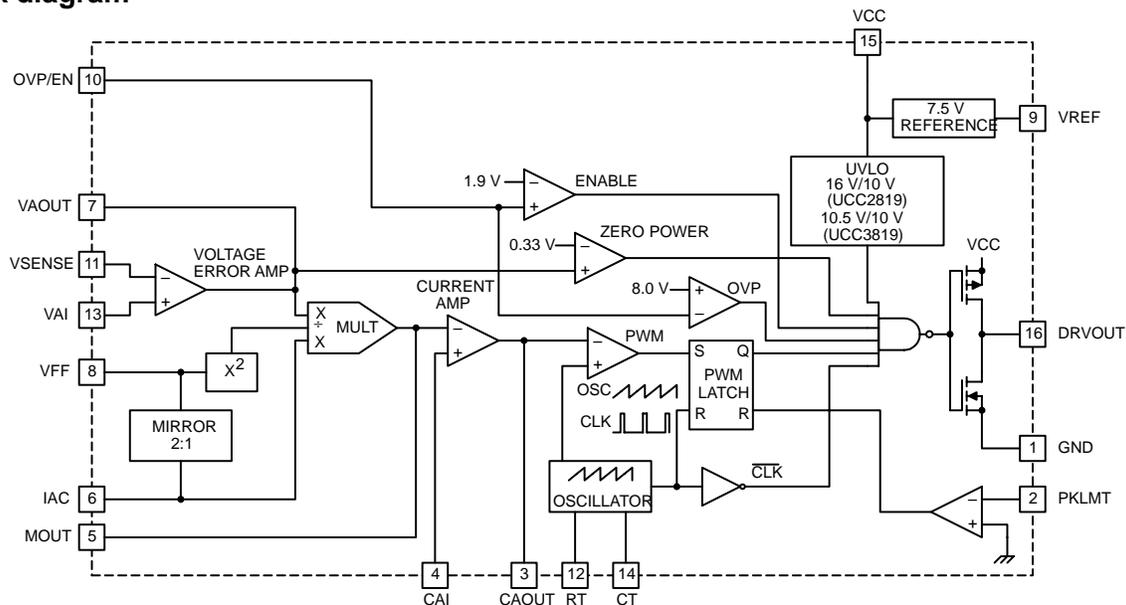
The UCC2819/UCC3819 provides all the functions necessary for active power factor corrected prerregulators. The controller achieves near unity power factor by shaping the ac-input line current waveform to correspond to that of the ac-input line voltage. Average current mode control maintains stable, low distortion sinusoidal line current.

Designed in Texas Instrument's BiCMOS process, the UCC3819 offers new features such as lower start-up current, lower power dissipation, overvoltage protection, a shunt UVLO detect circuitry and a leading-edge modulation technique to reduce ripple current in the bulk capacitor.

The UCC3819 allows the output voltage to be programmed by bringing out the error amplifier noninverting input.

Available in the 16-pin D, DW, N, and PW packages.

block diagram



UDG-01009



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

PRODUCTION DATA information is current as of publication date. Products conform to specifications per the terms of Texas Instruments standard warranty. Production processing does not necessarily include testing of all parameters.

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absolute maximum ratings over operating free-air temperature (unless otherwise noted)†

Supply voltage, VCC	18 V
Gate drive current, continuous	0.2 A
Gate drive current	1.2 A
Input voltage, CAI, MOUT	8 V
Input voltage, PKLMT	5 V
Input voltage, VSENSE, OVP/EN, VAI	10 V
Input current, RT, IAC, PKLMT	10 mA
Maximum negative voltage, DRVOUT, PKLMT, MOUT	-0.5 V
Power dissipation	1 W

† Stresses beyond those listed under “absolute maximum ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

AVAILABLE OPTIONS

T _J	PACKAGE DEVICES			
	D PACKAGE	DW PACKAGE	N PACKAGE	PW PACKAGE
0°C to 70°C	UCC3819D	UCC3819DW	UCC3819N	UCC3819PW
-40°C to 85°C	UCC2819D	UCC2819DW	UCC2819N	UCC2819PW

† The D, DW, and PW packages are available taped and reeled. Add TR suffix to device type (e.g. UCC3819DTR) to order quantities of 2500 devices per reel.

electrical characteristics, T_A = 0°C to 70°C for the UCC3819, -40°C to 85°C for the UCC2819, VCC = 12 V, R_T = 22 kΩ, C_T = 270 pF, (unless otherwise noted)

supply current

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Supply current, off	VCC = (VCC turnon threshold - 0.3 V)		150	300	μA
Supply current, on	VCC = 12 V, No load on DRVOUT	2	4	6	mA

UVLO

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
VCC turnon threshold		9.7	10.2	10.8	V
VCC turnoff threshold		9.4	9.7		V
UVLO hysteresis		0.3	0.5		V

voltage amplifier

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
V _{IO}	VAOUT = 2.75 V, VCM = 3.75 V	-15		15	mV
VAI bias current	VAOUT = 2.75 V, VCM = 3.75 V		50	200	nA
VSENSE bias current	VSENSE = VREF, VAOUT = 2.5 V		50	200	nA
CMRR	VCM = 1 V to 7.5 V	50	70		dB
Open loop gain	VAOUT = 2 V to 5 V	50	90		dB
High-level output voltage	I _L = -150 μA	5.3	5.5	5.6	V
Low-level output voltage	I _L = 150 μA	0	50	150	mV

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electrical characteristics, $T_A = 0^\circ\text{C}$ to 70°C for the UCC3819, -40°C to 85°C for the UCC2819, $V_{CC} = 12\text{ V}$, $R_T = 22\text{ k}\Omega$, $C_T = 270\text{ pF}$, (unless otherwise noted)

over voltage protection and enable

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Over voltage reference		$V_{REF} + 0.48$	$V_{REF} + 0.50$	$V_{REF} + 0.52$	V
Hysteresis		300	500	600	mV
Enable threshold		1.7	1.9	2.1	V
Enable hysteresis		0.1	0.2	0.3	V

current amplifier

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Input offset voltage	$V_{CM} = 0\text{ V}$, $V_{CAOUT} = 3\text{ V}$	-2	0	2	mV
Input bias current	$V_{CM} = 0\text{ V}$, $V_{CAOUT} = 3\text{ V}$		-50	-100	nA
Input offset current	$V_{CM} = 0\text{ V}$, $V_{CAOUT} = 3\text{ V}$		25	100	nA
Open loop gain	$V_{CM} = 0\text{ V}$, $V_{CAOUT} = 2\text{ V}$ to 5 V	90			dB
Common-mode rejection ratio	$V_{CM} = 0\text{ V}$ to 1.5 V , $V_{CAOUT} = 3\text{ V}$	60	80		dB
High-level output voltage	$I_L = -120\text{ }\mu\text{A}$	5.6	6.5	6.8	V
Low-level output voltage	$I_L = 1\text{ mA}$	0.1	0.2	0.5	V
Gain bandwidth product	See Note 1		2.5		MHz

voltage reference

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Input voltage, (UCC3819)	$T_A = 0^\circ\text{C}$ to 70°C	7.387	7.5	7.613	V
Input voltage, (UCC2819)	$T_A = -40^\circ\text{C}$ to 85°C	7.369	7.5	7.631	V
Load regulation	$I_{REF} = 1\text{ mA}$ to 2 mA	0		10	mV
Line regulation	$V_{CC} = 10.8\text{ V}$ to 15 V , See Note 2	0		10	mV
Short-circuit current	$V_{REF} = 0\text{ V}$	-20	-25	-50	mA

oscillator

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Initial accuracy	$T_A = 25^\circ\text{C}$	85	100	115	kHz
Voltage stability	$V_{CC} = 10.8\text{ V}$ to 15 V	-1		1	%
Total variation	Line, temp, See Note 1	80		120	kHz
Ramp peak voltage		4.5	5	5.5	V
Ramp amplitude voltage (peak to peak)		3.5	4	4.5	V

- NOTES: 1. Ensured by design, Not production tested.
2. Reference variation for $V_{CC} < 10.8\text{ V}$ is shown in Figure 2.

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electrical characteristics, $T_A = 0^\circ\text{C}$ to 70°C for the UCC3819, -40°C to 85°C for the UCC2819, $V_{CC} = 12\text{ V}$, $R_T = 22\text{ k}\Omega$, $C_T = 270\text{ pF}$, (unless otherwise noted)

peak current limit

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
PKLMT reference voltage		-15		15	mV
PKLMT propagation delay		150	350	500	ns

multiplier

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
I_{MOUT} ; high line, low power output current, (0°C to 85°C)	$I_{AC} = 500\text{ }\mu\text{A}$, $V_{FF} = 4.7\text{ V}$, $VA_{OUT} = 1.25\text{ V}$	0	-6	-20	μA
I_{MOUT} ; high line, low power output current, (-40°C to 85°C)	$I_{AC} = 500\text{ }\mu\text{A}$, $V_{FF} = 4.7\text{ V}$, $VA_{OUT} = 1.25\text{ V}$	0		-23	μA
I_{MOUT} ; high line, high power output current	$I_{AC} = 500\text{ }\mu\text{A}$, $V_{FF} = 4.7\text{ V}$, $VA_{OUT} = 5\text{ V}$	-70	-90	-105	μA
I_{MOUT} ; low line, low power output current	$I_{AC} = 150\text{ }\mu\text{A}$, $V_{FF} = 1.4\text{ V}$, $VA_{OUT} = 1.25\text{ V}$	-10	-19	-50	μA
I_{MOUT} ; low line, high power output current	$I_{AC} = 150\text{ }\mu\text{A}$, $V_{FF} = 1.4\text{ V}$, $VA_{OUT} = 5\text{ V}$	-268	-300	-346	μA
I_{MOUT} ; IAC limited	$I_{AC} = 150\text{ }\mu\text{A}$, $V_{FF} = 1.3\text{ V}$, $VA_{OUT} = 5\text{ V}$	-250	-300	-400	μA
Gain constant (K)	$I_{AC} = 300\text{ }\mu\text{A}$, $V_{FF} = 3\text{ V}$, $VA_{OUT} = 2.5\text{ V}$	0.5	1	1.5	1/V
I_{MOUT} ; zero current	$I_{AC} = 150\text{ }\mu\text{A}$, $V_{FF} = 1.4\text{ V}$, $VA_{OUT} = 0.25\text{ V}$		0	-2	μA
	$I_{AC} = 500\text{ }\mu\text{A}$, $V_{FF} = 4.7\text{ V}$, $VA_{OUT} = 0.25\text{ V}$		0	-2	μA
I_{MOUT} ; zero current, (0°C to 85°C)	$I_{AC} = 500\text{ }\mu\text{A}$, $V_{FF} = 4.7\text{ V}$, $VA_{OUT} = 0.5\text{ V}$		0	-3	μA
I_{MOUT} ; zero current, (-40°C to 85°C)	$I_{AC} = 500\text{ }\mu\text{A}$, $V_{FF} = 4.7\text{ V}$, $VA_{OUT} = 0.5\text{ V}$		0	-3.5	μA
Power limit ($I_{MOUT} \times V_{FF}$)	$I_{AC} = 150\text{ }\mu\text{A}$, $V_{FF} = 1.4\text{ V}$, $VA_{OUT} = 5\text{ V}$	-375	-420	-485	μW

feed-forward

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
VFF output current	$I_{AC} = 300\text{ }\mu\text{A}$	-140	-150	-160	μA

gate driver

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Pullup resistance	$I_O = -100\text{ mA}$ to -200 mA		5	12	Ω
Pulldown resistance	$I_O = 100\text{ mA}$		2	10	Ω
Output rise time	$C_L = 1\text{ nF}$, $R_L = 10\text{ }\Omega$, $V_{DRVOUT} = 0.7\text{ V}$ to 9 V		25	50	ns
Output fall time	$C_L = 1\text{ nF}$, $R_L = 10\text{ }\Omega$, $V_{DRVOUT} = 9\text{ V}$ to 0.7 V		10	50	ns
Maximum duty cycle		93	95	100	%
Minimum controlled duty cycle	At 100 kHz			2	%

zero power

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Zero power comparator threshold	Measured on VA_{OUT}	0.20	0.33	0.50	V

pin descriptions

CAI: (current amplifier noninverting input) Place a resistor between this pin and the GND side of current-sense resistor. This input and the inverting input (MOUT) remain functional down to and below GND.

CAOUT: (current amplifier output) This is the output of a wide bandwidth operational amplifier that senses line current and commands the PFC pulse-width modulator (PWM) to force the correct duty cycle. Compensation components are placed between CAOUT and MOUT.

CT: (oscillator timing capacitor) A capacitor from CT to GND sets the PWM oscillator frequency according to:

$$f \approx \left(\frac{0.6}{RT \times CT} \right)$$

The lead from the oscillator timing capacitor to GND should be as short and direct as possible.

DRVOUT: (gate drive) The output drive for the boost switch is a totem-pole MOSFET gate driver on DRVOUT. Use a series gate resistor to prevent interaction between the gate impedance and the output driver that might cause the DRVOUT to overshoot excessively. See characteristic curve (Figure 13) to determine minimum required gate resistor value. Some overshoot of the DRVOUT output is always expected when driving a capacitive load.

GND: (ground) All voltages measured with respect to ground. VCC and REF should be bypassed directly to GND with a 0.1-μF or larger ceramic capacitor.

IAC: (current proportional to input voltage) This input to the analog multiplier is a current proportional to instantaneous line voltage. The multiplier is tailored for very low distortion from this current input (I_{IAC}) to multiplier output. The recommended maximum I_{IAC} is 500 μA.

MOUT: (multiplier output and current amplifier inverting input) The output of the analog multiplier and the inverting input of the current amplifier are connected together at MOUT. As the multiplier output is a current, this is a high-impedance input so the amplifier can be configured as a differential amplifier. This configuration improves noise immunity and allows for the leading-edge modulation operation. The multiplier output current is limited to $(2 \times I_{IAC})$. The multiplier output current is given by the equation:

$$I_{MOUT} = \frac{I_{IAC} \times (V_{VAOUT} - 1)}{V_{VFF}^2 \times K}$$

where $K = \frac{1}{V}$ is the multiplier gain constant.

OVP/EN: (over-voltage/enable) A window comparator input that disables the output driver if the boost output voltage is a programmed level above the nominal or disables both the PFC output driver and resets SS if pulled below 1.9 V (typ).

PKLMT: (PFC peak current limit) The threshold for peak limit is 0 V. Use a resistor divider from the negative side of the current sense resistor to VREF to level shift this signal to a voltage level defined by the value of the sense resistor and the peak current limit. Peak current limit is reached when PKLMT voltage falls below 0 V.

RT: (oscillator charging current) A resistor from RT to GND is used to program oscillator charging current. A resistor between 10 kΩ and 100 kΩ is recommended. Nominal voltage on this pin is 3 V.

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pin descriptions (continued)

VAI: (voltage amplifier non-inverting input) This input can be tied to the VREF or any other voltage reference (≤ 7.5 V) to set the boost regulator output voltage.

VAOUT: (voltage amplifier output) This is the output of the operational amplifier that regulates output voltage. The voltage amplifier output is internally limited to approximately 5.5 V to prevent overshoot.

VCC: (positive supply voltage) Connect to a stable source of at least 20 mA between 10 V and 17 V for normal operation. Bypass VCC directly to GND to absorb supply current spikes required to charge external MOSFET gate capacitances. To prevent inadequate gate drive signals, the output devices are inhibited unless V_{VCC} exceeds the upper under-voltage lockout voltage threshold and remains above the lower threshold.

VFF: (feed-forward voltage) The RMS voltage signal generated at this pin by mirroring 1/2 of the I_{AC} into a single pole external filter. At low line, the VFF roll should be 14 V.

VSENSE: (voltage amplifier inverting input) This is normally connected to a compensation network and to the boost converter output through a divider network.

VREF: (voltage reference output) VREF is the output of an accurate 7.5-V voltage reference. This output is capable of delivering 20 mA to peripheral circuitry and is internally short-circuit current limited. VREF is disabled and remains at 0 V when V_{VCC} is below the UVLO threshold. Bypass VREF to GND with a 0.1- μ F or larger ceramic capacitor for best stability. Please refer to Figures 8 and 9 for VREF line and load regulation characteristics.

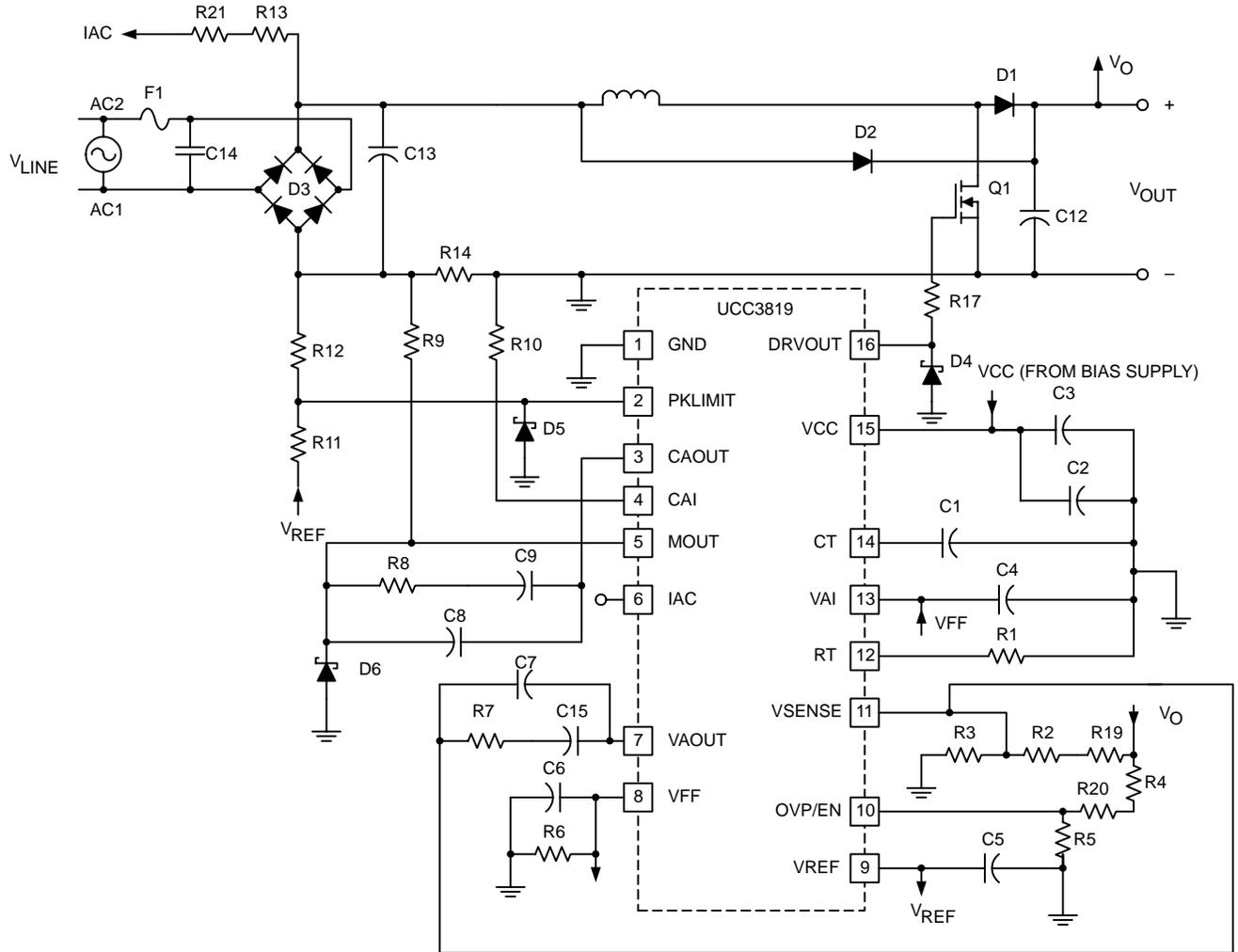
APPLICATION INFORMATION

The UCC3819 is based on the UCC3818 PFC preregulator. For a more detailed application information for this part, please refer to the UCC3818 datasheet product folder.

The main difference between the UCC3818 and the UCC3819 is that the non-inverting input of the voltage error amplifier is made available to the user through an external pin (VAI) in the UCC3819. The SS pin and function were eliminated to accommodate this change.

The benefit of VAI pin is that it can be used to dynamically change the PFC output voltage based on the line voltage (RMS) level or other conditions. Figure 1 shows one suggested implementation of the tracking boost PFC converter as this approach is sometimes referred to. The VAI pin is tied to the VFF pin and hence output voltage scales up with the line voltage. The benefit of this approach is that at lower line voltages the output voltage is lower and that leads to smaller boost inductor value, lower MOSFET conduction losses and reduced component stresses. In order for this feature to work, the downstream converter has to operate over a wider input range.

APPLICATION INFORMATION



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Figure 1. Suggested Implementation of UCC3819 in a Tracking Boost PFC Preregulator

APPLICATION INFORMATION

**REFERENCE VOLTAGE
 vs
 SUPPLY VOLTAGE**

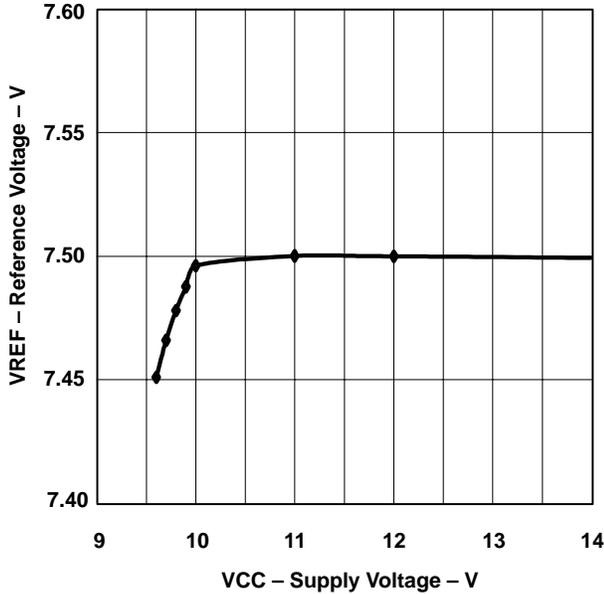


Figure 2

**REFERENCE VOLTAGE
 vs
 REFERENCE CURRENT**

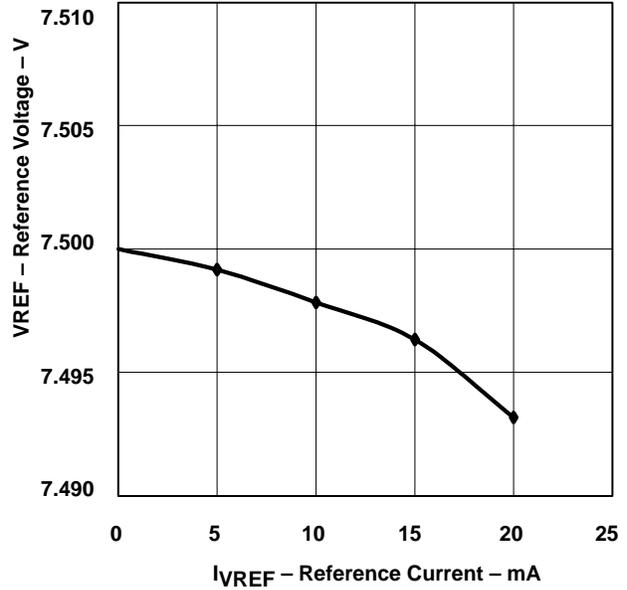


Figure 3

**MULTIPLIER OUTPUT CURRENT
 vs
 VOLTAGE ERROR AMPLIFIER OUTPUT**

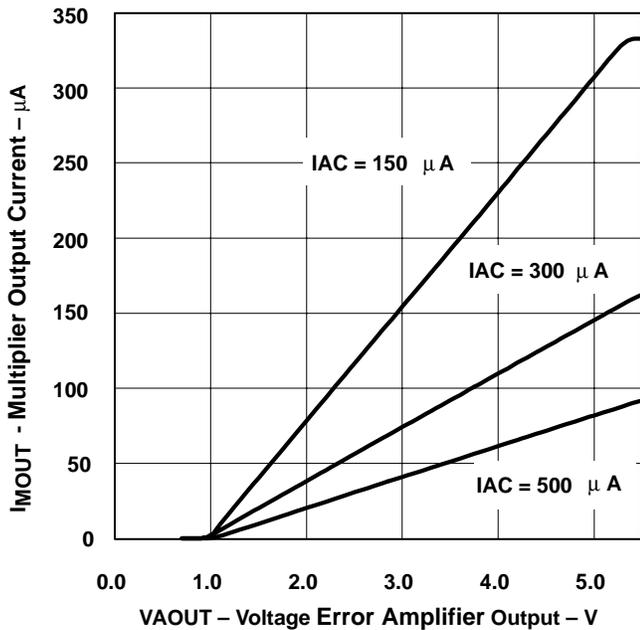


Figure 4

**MULTIPLIER GAIN
 vs
 VOLTAGE ERROR AMPLIFIER OUTPUT**

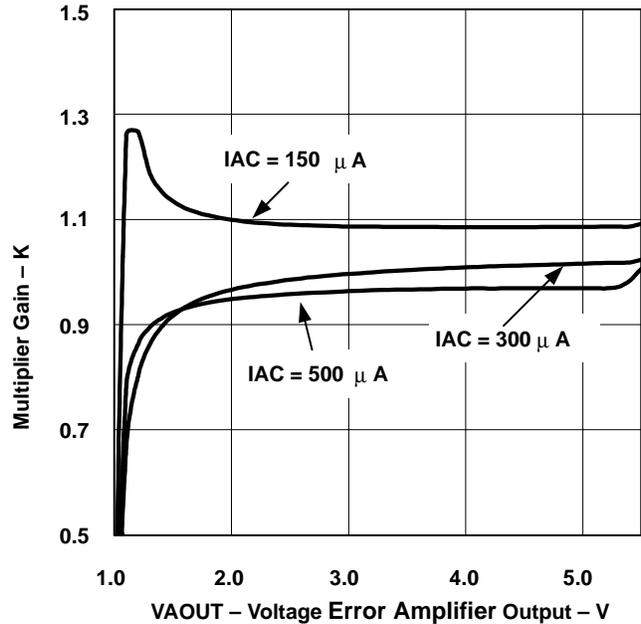


Figure 5

APPLICATION INFORMATION

MULTIPLIER CONSTANT POWER PERFORMANCE

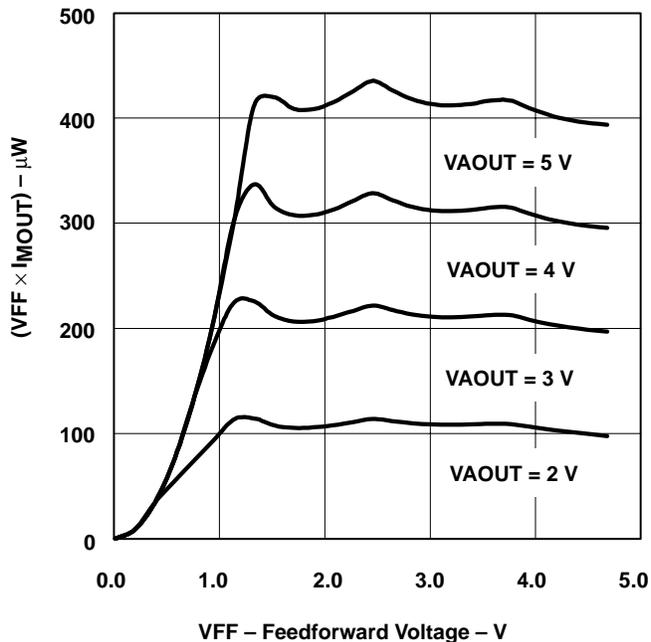


Figure 6

**RECOMMENDED MINIMUM GATE RESISTANCE
 VS
 SUPPLY VOLTAGE**

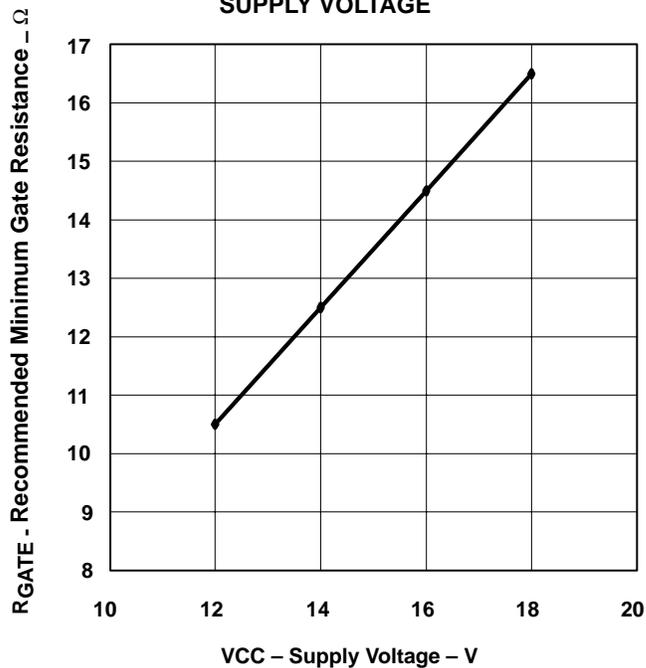


Figure 7

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