

SLVS416 - FEBRUARY 2002

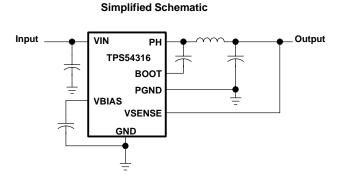
# 3-V TO 6-V INPUT, 3-A OUTPUT SYNCHRONOUS-BUCK PWM SWITCHER WITH INTEGRATED FETs (SWIFT™)

#### FEATURES

- 60-mΩ MOSFET Switches for High Efficiency at 3-A Continuous Output Source or Sink Current
- 0.9-V, 1.2-V, 1.5-V, 1.8-V, 2.5-V and 3.3-V Fixed Output Voltage Devices With 1% Initial Accuracy
- Internally Compensated for Ease of Use and Minimal Component Count
- Fast Transient Response
- Wide PWM Frequency—Fixed 350 kHz, 550 kHz or Adjustable 280 kHz to 700 kHz
- Load Protected by Peak Current Limit and Thermal Shutdown
- Integrated Solution Reduces Board Area and Total Cost

#### APPLICATIONS

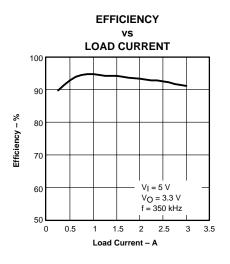
- Low-Voltage, High-Density Systems With Power Distributed at 5 V or 3.3 V
- Point of Load Regulation for High-Performance DSPs, FPGAs, ASICs, and Microprocessors
- Broadband, Networking, and Optical Communications Infrastructure
- Portable Computing/Notebook PCs



#### DESCRIPTION

As members of the SWIFT<sup>TM</sup> family of dc/dc regulators, the TPS54311, TPS54312, TPS54313, TPS54314, TPS54315 and TPS54316 low-input-voltage highoutput-current synchronous-buck PWM converters integrate all required active components. Included on the substrate with the listed features are a true, high performance, voltage error amplifier that provides fast response under transient conditions; an undervoltagelockout circuit to prevent start-up until the input voltage reaches 3 V; an internally and externally set slow-start circuit to limit in-rush currents; and a power good output useful for processor/logic reset, fault signaling and supply sequencing.

The TPS54311-6 devices are available in a thermally enhanced 20-pin TSSOP (PWP) PowerPAD<sup>™</sup> package, which eliminates bulky heatsinks. TI provides evaluation modules and the SWIFT<sup>™</sup> designer software tool to aid in quickly achieving high-performance power supply designs to meet aggressive equipment development cycles.





Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

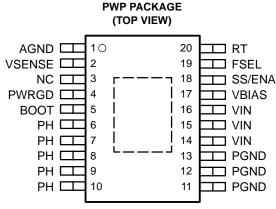
SWIFT and PowerPAD are trademarks of Texas Instruments.







This device contains circuits to protect its inputs and outputs against damage due to high static voltages or electrostatic fields. These circuits have been qualified to protect this device against electrostatic discharges (ESD) of up to 2 kV according to MIL-STD-883C, Method 3015; however, it is advised that precautions should be taken to avoid application of any voltage higher than maximum-rated voltages to these high-impedance circuits. During storage or handling, the device leads should be shorted together or the device should be placed in conductive foam. In a circuit, unused inputs should always be connected to an appropriated logic voltage level, preferably either V<sub>CC</sub> or ground. Specific guidelines for handling devices of this type are contained in the publication *Guidelines for Handling Electrostatic-Discharge-Sensitive (ESDS) Devices and Assemblies* available from Texas Instruments.



NC – No internal connection

#### **AVAILABLE OPTIONS**

Tj	OUTPUT VOLTAGE	PACKAGED DEVICES PLASTIC HTSSOP (PWP) <sup>†</sup>	Tj	OUTPUT VOLTAGE	PACKAGED DEVICES PLASTIC HTSSOP (PWP) <sup>†</sup>
	0.9 V	TPS54311PWP		1.8 V	TPS54314PWP
-40°C to 125°C	1.2 V	TPS54312PWP	-40°C to 125°C	2.5 V	TPS54315PWP
	1.5 V	TPS54313PWP		3.3 V	TPS54316PWP

<sup>†</sup> The PWP package is also available taped and reeled. Add an R suffix to the device type (i.e., TPS54316PWPR). See application section of datasheet for PowerPAD<sup>™</sup> drawing and layout information.

#### **Terminal Functions**

TERMINAL		1/0	DESCRIPTION		
NAME	NO.	1/0	DESCRIPTION		
AGND	1		Analog ground. Return for compensation network/output divider, slow start capacitor, VBIAS capacitor, RT resistor and FSEL pin. Make PowerPad <sup>TM</sup> connection to AGND.		
BOOT	5		Bootstrap input. 0.022 $\mu$ F to 0.1 $\mu$ F low ESR capacitor connected from BOOT to PH generates floating drive for the high-set FET driver.		
FSEL	19		Frequency select input. Provides logic input to select between two internally set switching frequencies.		
NC	3		No connection		
PGND	11–13		Power ground. High current return for the low-side driver and power MOSFET. Connect PGND with large copper areas to the input and output supply returns, and negative terminals of the input and output capacitors.		
PH	6–10		Phase input/output. Junction of the internal high- and low-side power MOSFETs, and output inductor.		
PWRGD	4		Powergood open drain output. Hi-Z when VSENSE ≥90% VREF, otherwise PWRGD is low. Note that output is low when SS/ENA is low or internal shutdown signal active.		
RT	20		Frequency setting resistor input. Connect a resistor from RT to AGND to set the switching frequency, Fs.		
SS/ENA	18		Slow start/enable input/output. Dual function pin which provides logic input to enable/disable device operation and capacitor input to externally set the start-up time.		
VBIAS	17		Internal bias regulator output. Supplies regulated voltage to internal circuitry. Bypass VBIAS pin to AGND pin with a high quality, low ESR 0.1 $\mu$ F to 1.0 $\mu$ F ceramic capacitor.		
VIN	14–16		Input supply for the power MOSFET switches and internal bias regulator. Bypass VIN pins to PGND pins close to device package with a high quality, low ESR 1 $\mu$ F to 10 $\mu$ F ceramic capacitor.		
VSENSE	2		Error amplifier inverting input. Connect directly to output voltage sense point.		



## absolute maximum ratings over operating virtual junction temperature range (unless otherwise noted) $\!\!\!\!^\dagger$

Input voltage range, V <sub>I</sub> : VIN, SS/ENA, FSEL	–0.3 V to 7 V
RT	
VSENSE	–0.3 V to 4 V
BOOT	–0.3 V to 17 V
Output voltage range, V <sub>O</sub> : VBIAS, PWRGD	$\ldots$ –0.3 V to 7 V
PH	
Source current, I <sub>O</sub> : PH	Internally Limited
VBIAS	
Sink current, I <sub>S</sub> : PH	
SS/ENA, PWRGD	10 mA
Voltage differential: AGND to PGND	±0.3 V
Continuous power dissipation	See Power Dissipation Rating Table
Operating virtual junction temperature range, T <sub>J</sub>	
Storage temperature, T <sub>stg</sub>	–65°C to 150°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds	300°C

<sup>†</sup> Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

#### DISSIPATION RATING TABLE<sup>‡</sup>

PACKAGE	THERMAL IMPEDANCE JUNCTION-TO-AMBIENT	T <sub>A</sub> = 25°C POWER RATING	T <sub>A</sub> = 70°C POWER RATING	T <sub>A</sub> = 85°C POWER RATING
20-Pin PWP with solder	26.0 mW/°C	3.85 W§	2.12 W	1.54 W
20-Pin PWP without solder	57.5 mW/°C	1.73 W	0.96 W	0.69 W

<sup>‡</sup> Test board conditions:

1. 3" x 3", 2 layers, Thickness: 0.062"

2. 1.5 oz. copper traces located on the top of the PCB

3. 1.5 oz. copper ground plane on the bottom of the PCB

4. 10 thermal vias (see Recommended Land Pattern in applications section of this data sheet)

For more information on the PWP package, refer to TI technical brief, literature number SLMA002.

§ Maximum power dissipation may be limited by over current protection.

#### ADDITIONAL 3A SWIFT<sup>TM</sup> DEVICES

DEVICE	OUTPUT VOLTAGE		
TPS54310	0.9 V to 3.3 V		

#### related dc/dc products

- UCC3585—dc/dc controller
- PT5500 series—3-A plug-in modules
- TPS757xx—3-A low dropout regulator



## electrical characteristics, $T_J = -40^{\circ}C$ to $125^{\circ}C$ , $V_I = 3$ V to 6 V (unless otherwise noted)

	PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY \	/OLTAGE, VIN			1			
	Input voltage range at V	/IN		3.0		6.0	V
	Quiescent current		Fs = 350 kHz, FSEL $\leq$ 0.8 V, RT open, Phase pin open		6.2	9.6	mA
lQ			Fs = 550 kHz, FSEL ≥ 2.5 V, RT open, Phase pin open		8.4	12.8	mA
			Shutdown, SS/ENA = 0 V		1	1.4	mA
UNDER V	OLTAGE LOCK OUT						
VIT(start)	Start threshold voltage	at UVLO			2.95	3.0	V
VIT(stop)	Stop threshold voltage	at UVLO		2.70	2.80		V
V <sub>hys</sub>	Hysteresis voltage at U	VLO		0.14	0.16		V
t <sub>f</sub> , t <sub>r</sub>	Rising and falling edge	deglitch at UVLO	See Note 1		2.5		μs
BIAS VOL	TAGE		·				
	Output voltage at VBIA	S	$I_{VBIAS} = 0$	2.70	2.80	2.90	V
	Output current at VBIAS		See Note 2			100	μA
OUTPUT	VOLTAGE		·				
	Output voltage		$T_{J} = 25^{\circ}C,$ VIN = 5.0 V		0.9		V
		TPS54311	$3 \leq \text{VIN} \leq 6 \text{ V},  0 \leq \text{IL} \leq 3\text{A},  -40 \leq T_J \leq 125$	-2.5%		2.5%	
		TPS54312	$T_J = 25^{\circ}C, VIN = 5.0 V$		1.2		V
			$3 \leq VIN \leq 6 \text{ V},  0 \leq IL \leq 3 \text{ A},  -40 \leq T_J \leq 125$	-2.5%		2.5%	
		TPS54313	$T_{J} = 25^{\circ}C, VIN = 5.0V$		1.5		V
			$3 \leq VIN \leq 6 \ V,  0 \leq IL \leq 3 \ A,  -40 \leq T_J \leq 125$	-2.5%		2.5%	
VO		TPS54314	$T_{J} = 25^{\circ}C, VIN = 5.0 V$		1.8		V
			$3 \le VIN \le 6 V,  0 \le IL \le 3 A,  -40 \le T_J \le 125$	-3%		3%	
		70054045	T <sub>J</sub> = 25°C, VIN = 5.0V		2.5		V
		TPS54315	$3 \leq VIN \leq 6 \text{ V},  0 \leq IL \leq 3 \text{ A},  -40 \leq T_J \leq 125$	-3%		3%	
		TD054040	T <sub>J</sub> = 25°C, VIN = 5.0V		3.3		V
		TPS54316	$3 \leq VIN \leq 6~V,  0 \leq IL \leq 3~A,  -40 \leq T_J \leq 125$	-3%		3%	
REGULAT	TION						
Line regulation			IL = 1.5A, $350 \le \text{fs} \le 550 \text{ kHz}$ , TJ = $85^{\circ}\text{C}$ , See Note 1, 3			0.21	%/V
Load regulation			IL = 0 to 3A, $350 \le \text{fs} \le 550 \text{ kHz}$ , TJ = $85^{\circ}$ C, See Notes 1 and 3			0.21	%/A

NOTES: 1. Ensured by design

2. Static resistive loads only

3. Tested using circuit in Figure 9



## TPS54311, TPS54312 TPS54313, TPS54314 **TPS54315, TPS54316** SLVS416 – FEBRUARY 2002

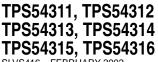
### electrical characteristics, $T_J = -40^{\circ}C$ to $125^{\circ}C$ , $V_I = 3$ V to 6 V (unless otherwise noted)(continued)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
OSCILLATOR					
	SYNC<=0.8 V, RT open	280	350	420	
Internally set-free running frequency	SYNC>= 2.5V, RT open	440	550	660	kHz
	RT = 180 k $\Omega$ (1% resistor to AGND)	252	280	308	
Externally set-free running frequency range	RT = 100 k $\Omega$ (1% resistor to AGND)	460	500	540	kHz
	RT = 68 k $\Omega$ (1% resistor to AGND)	663	700	762	
High level threshold at FSEL		2.5			V
Low level threshold at FSEL				0.8	V
Ramp valley	See Note 1		0.75		V
Ramp amplitude (peak to peak)	See Note 1		1		V
Minimum controllable on time	See Note 1			200	nS
Maximum duty cycle	See Note 1	90%			
ERROR AMPLIFIER	-				
Error amplifier open loop voltage gain	See Note 1		26		dB
Error amplifier unity gain bandwidth	See Note 1	3	5		MHz
Error amplifier common mode input voltage range	Powered by internal LDO, See Note 1	0		Vbias	V
PWM COMPARATOR	-				
PWM comparator propagation delay time, PWM comparator input to PH pin (excluding dead time)	10 mV overdrive, See Note 1		70	85	ns
SLOW START / ENABLE					
Enable threshold voltage at SS/ENA		0.95	1.20	1.40	V
Enable hysteresis voltage at SS/ENA	See Note 1		0.03		V
Falling edge deglitch at SS/ENA	See Note 1		2.5		μs
Internal slow-start time		2.6	3.35	4.1	ms
Charge current at SS/ENA	SS/ENA = 0V	3	5	8	μA
Discharge current at SS/ENA	SS/ENA = 1.3 V, V <sub>IN</sub> = 1.5 V	1.5	2.3	4.0	mA
POWER GOOD					
Power good threshold voltage	VSENSE falling		90		%Vout
Power good hysteresis voltage	See Note 1		3		%Vout
Power good falling edge deglitch	See Note 1		35		μs
Output saturation voltage at PWRGD	I <sub>sink</sub> = 2.5 mA		0.18	0.30	V
Leakage current, PWRGD	V <sub>IN</sub> = 5.5 V			1	μA
CURRENT LIMIT	1 ···				
	V <sub>IN</sub> = 3 V (see Note 1)	4.0	6.5		
Current limit	V <sub>IN</sub> = 6 V (see Note 1)	4.5	7.5		A
Current limit leading edge blanking time			100		ns
Current limit total response time			200		ns
THERMAL SHUTDOWN	•				•
Thermal shutdown trip point	See Note 1	135	150	165	°C
Thermal shutdown hysteresis	See Note 1	1	10		°C
OUTPUT POWER MOSFETS	•	•			<u>n</u>
Small signal drain-source on power MOSFET switches	I <sub>O</sub> = 3A, V <sub>IN</sub> = 6.0 V See Note 4		59	88	
RDS-ON	I <sub>O</sub> = 3A, V <sub>IN</sub> = 3.0 V See Note 4		85	136	mΩ

NOTES: 3: Tested using circuit in Figure 9

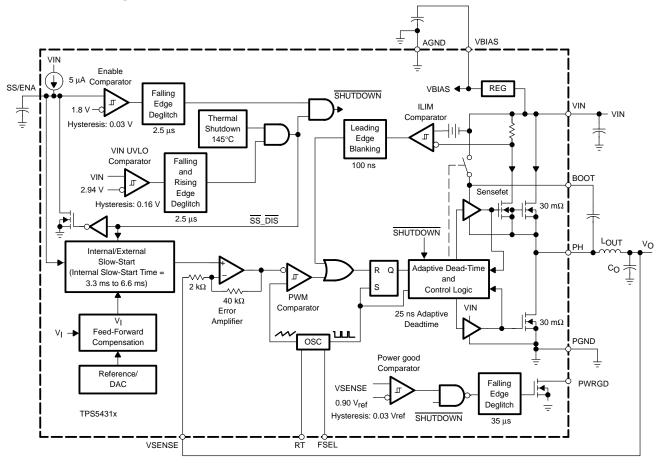
4. Matched MOSFETs, low side RDS-ON production tested, high side RDS-ON ensured by design





SLVS416 – FEBRUARY 2002

#### internal block diagram



#### detailed description

#### undervoltage lock out (UVLO)

An under voltage lockout circuit to keep the device disabled when the input voltage (VIN) is insufficient. During power up, internal circuits are held inactive until VIN exceeds the nominal UVLO threshold voltage of 2.95 V. Once the UVLO start threshold is reached, device start-up begins. The device operates until VIN falls below the nominal UVLO stop threshold of 2.8 V. Hysteresis in the UVLO comparator, and a 2.5 µs rising and falling edge deglitch circuit reduce the likelihood of shutting the device down due to noise on VIN.

#### slow-start/enable (SS/ENA)

The slow-start/enable pin provides two functions. First, the pin acts as an enable (shutdown) control by keeping the device turned off until the voltage exceeds the start threshold voltage of approximately 1.2 V. When SS/ENA exceeds the enable threshold, device start-up begins. The reference voltage fed to the error amplifier is linearly ramped up from 0 V to 0.891 V in 3.35 ms. Similarly, the converter output voltage reaches regulation in approximately 3.35 ms. Voltage hysteresis and a 2.5  $\mu$ s falling edge deglitch circuit reduce the likelihood of triggering the enable due to noise.



#### slow-start/enable (SS/ENA) (continued)

The second function of the SS/ENA pin provides an external means of extending the slow-start time with a low-value capacitor connected between SS/ENA and AGND. Adding a capacitor to the SS/ENA pin has two effects on start-up. First, a delay occurs between release of the SS/ENA pin and start-up of the output. The delay is proportional to the slow-start capacitor value and lasts until the SS/ENA pin reaches the enable threshold. The start-up delay is approximately:

$$t_{d} = C_{(SS)} \times \left(\frac{1.2 \text{ V}}{5 \,\mu\text{A}}\right) \tag{1}$$

Second, as the output becomes active, a brief ramp-up at the internal slow-start rate may be observed before the externally set slow-start rate takes control and the output rises at a rate proportional to the slow-start capacitor. The slow-start time set by the capacitor is approximately:

$$t_{(SS)} = C_{(SS)} \times \left(\frac{0.7 \text{ V}}{5 \,\mu\text{A}}\right)$$
(2)

The actual slow-start time is likely to be less than the above approximation due to the brief ramp-up at the internal rate.

#### VBIAS regulator (VBIAS)

The VBIAS regulator provides internal analog and digital blocks with a stable supply voltage over variations in junction temperature and input voltage. A high quality, low-ESR, ceramic bypass capacitor is required on the VBIAS pin. X7R or X5R grade dielectrics are recommended because their values are more stable over temperature. The bypass capacitor should be placed close to the VBIAS pin and returned to AGND. External loading on VBIAS is allowed, with the caution that internal circuits require a minimum VBIAS of 2.70 V, and external loads on VBIAS with ac or digital switching noise may degrade performance. The VBIAS pin may be useful as a reference voltage for external circuits.

#### voltage reference

The voltage reference system produces a precise, temperature stable voltage from a bandgap circuit. A scaling amplifier and DAC are then used to produce the reference voltages for each of the fixed output devices

#### oscillator and PWM ramp

The oscillator frequency can be set to internally fixed values of 350 kHz or 550 kHz using the FSEL pin as a static digital input. If a different frequency of operation is required for the application, the oscillator frequency can be externally adjusted from 280 to 700 kHz by connecting a resistor from the RT pin to AGND and floating the FSEL pin. The switching frequency is approximated by the following equation, where R is the resistance from RT to AGND:

SWITCHING FREQUENCY = 
$$\left(\frac{100 \text{ k}\Omega}{\text{RT}}\right) \times 500 \text{ kHz}$$
 (3)

The following table summarizes the frequency selection configurations:

SWITCHING FREQUENCY	SYNC PIN	RT PIN
350 kHz, internally set	Float or AGND	Float
550 kHz, internally set	$\geq$ 2.5 V	Float
Externally set 280 kHz to 700 kHz	Float	R = 180 k to 68 k



#### detailed description (continued)

#### error amplifier

The high performance, wide bandwidth, voltage error amplifier is gain limited to provide internal compensation of the control loop. The user is given limited flexibility in choosing output L and C filter components. Inductance values of 4.7  $\mu$ H to 10  $\mu$ H are typical and available from several vendors. The resulting designs exhibit good noise and ripple characteristics, along with exceptional transient response. Transient recovery times are typically in the range of 10 to 20  $\mu$ s.

#### **PWM control**

Signals from the error amplifier, oscillator and current limit circuit are processed by the PWM control logic. Referring to the internal block diagram, the control logic includes the PWM comparator, OR gate, PWM latch, and portions of the adaptive dead-time and control logic block. During steady-state operation below the current limit threshold, the PWM comparator output and oscillator pulse train alternately reset and set the PWM latch. Once the PWM latch is reset, the low-side FET remains on for a minimum duration set by the oscillator pulse width. During this period, the PWM ramp discharges rapidly to its valley voltage. When the ramp begins to charge back up, the low-side FET turns off and high-side FET turns on. As the PWM ramp voltage exceeds the error amplifier output voltage, the PWM comparator resets the latch, thus turning off the high-side FET and turning on the low-side FET. The low-side FET remains on until the next oscillator pulse discharges the PWM ramp.

During transient conditions, the error amplifier output could be below the PWM ramp valley voltage or above the PWM peak voltage. If the error amplifier is high, the PWM latch is never reset and the high-side FET remains on until the oscillator pulse signals the control logic to turn the high-side FET off and the low-side FET on. The device operates at its maximum duty cycle until the output voltage rises to the regulation set-point, setting VSENSE to approximately the same voltage as  $V_{REF}$ . If the error amplifier output is low, the PWM latch is continually reset and the high-side FET does not turn on. The low-side FET remains on until the VSENSE voltage decreases to a range that allows the PWM comparator to change states. The TPS54611–TPS54616 devices are capable of sinking current continuously until the output reaches the regulation set-point.

If the current limit comparator trips for longer than 100 ns, the PWM latch resets before the PWM ramp exceeds the error amplifier output. The high-side FET turns off and low-side FET turns on to decrease the energy in the output inductor and consequently the output current. This process is repeated each cycle in which the current limit comparator is tripped.

#### dead-time control and MOSFET drivers

Adaptive dead-time control prevents shoot-through current from flowing in both N-channel power MOSFETs during the switching transitions by actively controlling the turnon times of the MOSFET drivers. The high-side driver does not turn on until the voltage at the gate of the low-side FET is below 2 V. While the low-side driver does not turn on until the voltage at the gate of the high-side MOSFET is below 2 V. The high-side and low-side drivers are designed with 300-mA source and sink capability to quickly drive the power MOSFETs gates. The low-side driver is supplied from VIN, while the high-side drive is supplied from the BOOT pin. A bootstrap circuit uses an external BOOT capacitor and an internal  $2.5 \Omega$  bootstrap switch connected between the VIN and BOOT pins. The integrated bootstrap switch improves drive efficiency and reduces external component count.

#### overcurrent protection

The cycle by cycle current limiting is achieved by sensing the current flowing through the high-side MOSFET and a differential amplifier with preset overcurrent threshold. The high side MOSFET is turned off within 200 ns of reaching the current limit threshold. A 100-ns leading edge blanking circuit prevents false tripping of current limit. Current limit detection occurs only when current flows from VIN to PH when sourcing current to the output filter. Load protection during current sink operation is provided by thermal shutdown.





#### detailed description (continued)

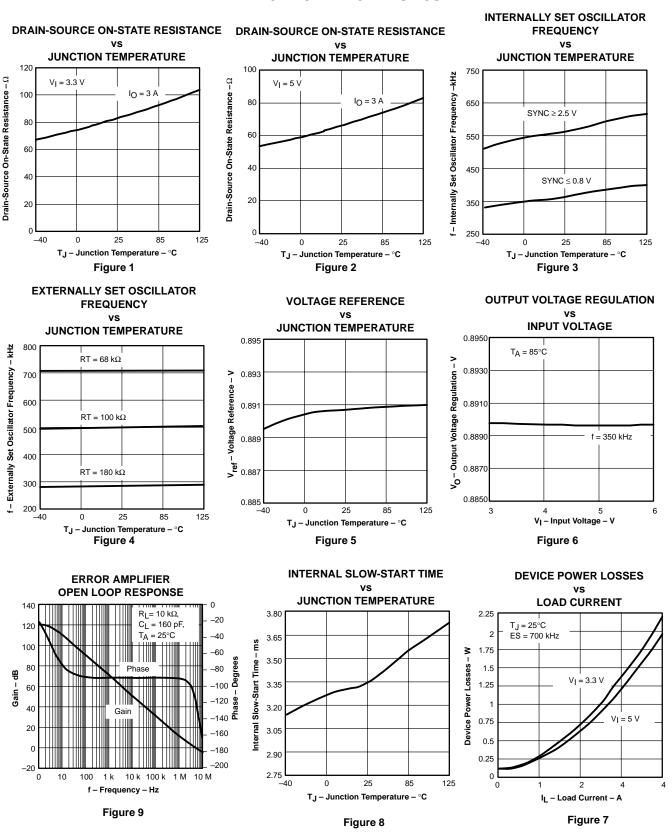
#### thermal shutdown

The device uses the thermal shutdown to turn off the power MOSFETs and disable the controller if the junction temperature exceeds 150°C. The device is released from shutdown when the junction temperature decreases to 10°C below the thermal shutdown trip point, and will start up under control of the slow-start circuit. Thermal shutdown provides protection when an overload condition is sustained for several milliseconds. With a persistent fault condition, the device will cycle continuously: starting up by control of the soft-start circuit, heating up due to the fault, and then shutting down upon reaching the thermal shutdown trip point.

#### power good (PWRGD)

The power good circuit monitors for under voltage conditions on VSENSE. If the voltage on VSENSE is 10% below the reference voltage, the open-drain PWRGD output is pulled low. PWRGD is also pulled low if VIN is less than the UVLO threshold or SS/ENA is low, or thermal shutdown is asserted. When VIN = UVLO threshold, SS/ENA = enable threshold, and VSENSE > 90% of V<sub>ref</sub>, the open drain output of the PWRGD pin is high. A hysteresis voltage equal to 3% of V<sub>ref</sub> and a 35  $\mu$ s falling edge deglitch circuit prevent tripping of the power good comparator due to high frequency noise.





## TYPICAL CHARACTERISTICS



#### **APPLICATION INFORMATION**

Figure 10 shows the schematic diagram for a typical TPS54314 application. The TPS54314 (U1) can provide up to 3 A of output current at a nominal output voltage of 1.8 V. For proper thermal performance, the power pad underneath the integrated circuit TPS54314 needs to be soldered well to the printed-circuit board.

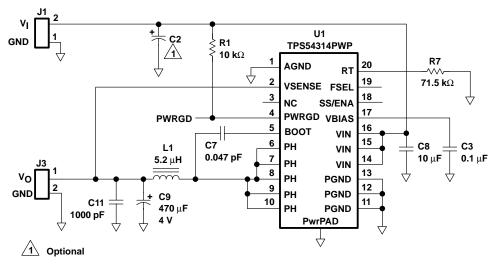


Figure 10. TPS54314 Schematic

#### input voltage

The input to the circuit is a nominal 5 VDC, applied at J1. The optional input filter (C2) is a 220–uF POSCAP capacitor, with a maximum allowable ripple current of 3 A. C8 is the decoupling capacitor for the TPS54314 and must be located as close to the device as possible.

#### feedback circuit

The output voltage of the converter is fed directly into the VSENSE pin of the TPS54314. The TPS54314 is internally compensated to provide stability of the output under varying line and load conditions.

#### operating frequency

In the application circuit, a 700 kHz operating frequency is selected by leaving FSEL open and connecting a 71.5 k $\Omega$  resistor between the RT pin and AGND. Different operating frequencies may be selected by varying the value of R3 using equation 4:

$$R = \frac{500 \text{ kHz}}{\text{Switching Frequency}} \times 100 \text{ k}\Omega$$
(4)

Alternately, preset operating frequencies of 350 kHz or 550 kHz my be selected by leaving RT open and connecting the FSEL pin to AGND or Vin respectively.

#### output filter

The output filter is composed of a 5.2  $\mu$ H inductor and 470  $\mu$ F capacitor. The inductor is a low dc resistance(16-m $\Omega$ ) type, Sumida CDRH104R–5R2. The capacitor used is a 4-V POSCAP with a maximum ESR of 40 m $\Omega$ . The output filter components work with the internal compensation network to provide a stable closed loop response for the converter.



#### **APPLICATION INFORMATION**

#### grounding and PowerPAD layout

The TPS54311–16 have two internal grounds (analog and power). Inside the TPS54311–16, the analog ground ties to all of the noise sensitive signals, while the power ground ties to the noisier power signals. The PowerPAD must be connected directly to AGND. Noise injected between the two grounds can degrade the performance of the TPS54311–16, particularly at higher output currents. However, ground noise on an analog ground plane can also cause problems with some of the control and bias signals. For these reasons, separate analog and power ground planes are recommended. These two planes should tie together directly at the IC to reduce noise between the two grounds. The only components that should tie directly to the power ground plane are the input capacitor, the output capacitor, the input voltage decoupling capacitor, and the PGND pins of the TPS54311–16. The layout of the TPS54314 evaluation module is representative of a recommended layout for a 4-layer board. Documentation for the TPS54314 evaluation module can be found on the Texas Instruments web site under the TPS54314 product folder and in the application note, TI literature number SLVA111.

#### layout considerations for thermal performance

For operation at full rated load current, the analog ground plane must provide adequate heat dissipating area. A 3 inch by 3 inch plane of 1 ounce copper is recommended, though not mandatory, depending on ambient temperature and airflow. Most applications have larger areas of internal ground plane available, and the PowerPAD should be connected to the largest area available. Additional areas on the top or bottom layers also help dissipate heat, and any area available should be used when 3 A or greater operation is desired. Connection from the exposed area of the PowerPAD to the analog ground plane layer should be made using 0.013 inch diameter vias to avoid solder wicking through the vias. Six vias should be in the PowerPAD area with four additional vias located under the device package. The size of the vias under the package, but not in the exposed thermal pad area, can be increased to 0.018. Additional vias beyond the ten recommended that enhance thermal performance should be included in areas not under the device package.

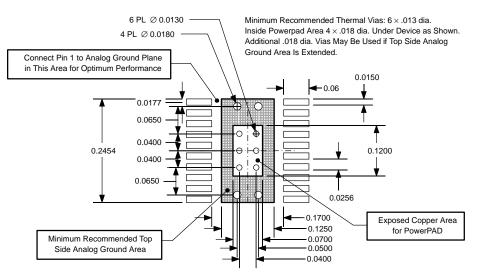
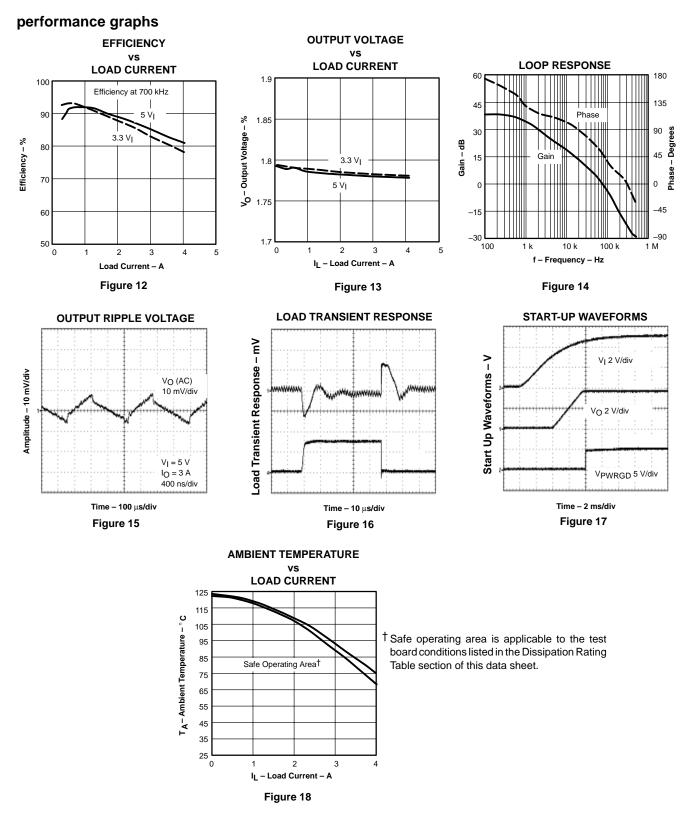


Figure 11. Recommended Land Pattern for 20-Pin PWP PowerPAD



#### **APPLICATION INFORMATION**



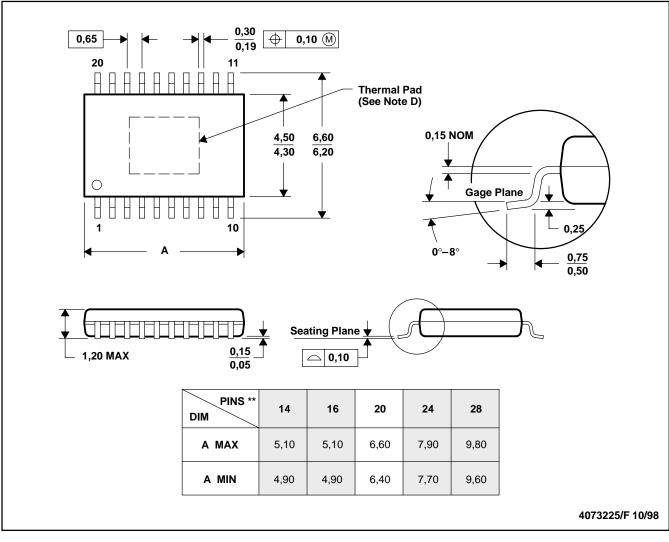


**MECHANICAL DATA** 

#### PWP (R-PDSO-G\*\*)

**PowerPAD™ PLASTIC SMALL-OUTLINE** 

#### **20 PINS SHOWN**



NOTES: A. All linear dimensions are in millimeters.

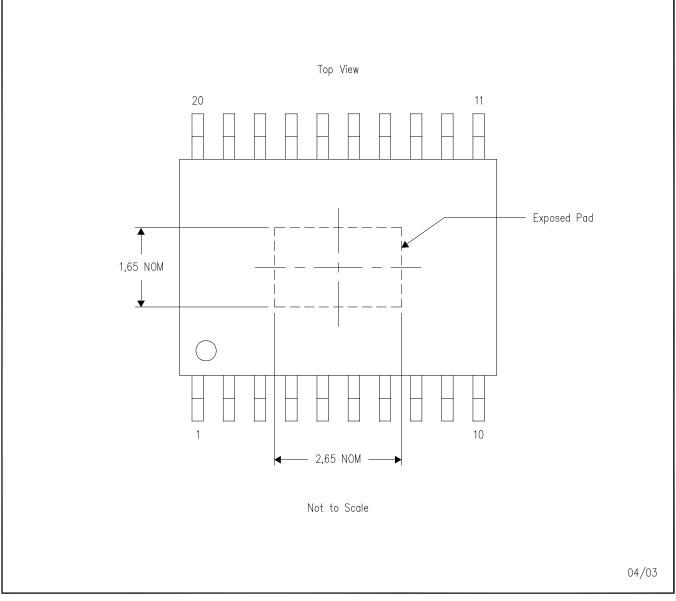
- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusions.
- D. The package thermal performance may be enhanced by bonding the thermal pad to an external thermal plane. This pad is electrically and thermally connected to the backside of the die and possibly selected leads.
- E. Falls within JEDEC MO-153

PowerPAD is a trademark of Texas Instruments.



#### PWP (R-PDSO-G20)

#### PowerPAD<sup>™</sup> PLASTIC SMALL-OUTLINE



NOTES: A. All linear dimensions are in millimeters.

B. This drawing is subject to change without notice.

PowerPAD is a trademark of Texas Instruments Incorporated.



C. For additional information on the PowerPAD<sup>™</sup> package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, *PowerPAD Thermally Enhanced Package*, Texas Instruments Literature No. SLMA002 and Application Brief, *PowerPAD Made Easy*, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

#### **IMPORTANT NOTICE**

Texas Instruments Incorporated and its subsidiaries (TI) reserve the right to make corrections, modifications, enhancements, improvements, and other changes to its products and services at any time and to discontinue any product or service without notice. Customers should obtain the latest relevant information before placing orders and should verify that such information is current and complete. All products are sold subject to TI's terms and conditions of sale supplied at the time of order acknowledgment.

TI warrants performance of its hardware products to the specifications applicable at the time of sale in accordance with TI's standard warranty. Testing and other quality control techniques are used to the extent TI deems necessary to support this warranty. Except where mandated by government requirements, testing of all parameters of each product is not necessarily performed.

TI assumes no liability for applications assistance or customer product design. Customers are responsible for their products and applications using TI components. To minimize the risks associated with customer products and applications, customers should provide adequate design and operating safeguards.

TI does not warrant or represent that any license, either express or implied, is granted under any TI patent right, copyright, mask work right, or other TI intellectual property right relating to any combination, machine, or process in which TI products or services are used. Information published by TI regarding third–party products or services does not constitute a license from TI to use such products or services or a warranty or endorsement thereof. Use of such information may require a license from a third party under the patents or other intellectual property of the third party, or a license from TI under the patents or other intellectual property of TI.

Reproduction of information in TI data books or data sheets is permissible only if reproduction is without alteration and is accompanied by all associated warranties, conditions, limitations, and notices. Reproduction of this information with alteration is an unfair and deceptive business practice. TI is not responsible or liable for such altered documentation.

Resale of TI products or services with statements different from or beyond the parameters stated by TI for that product or service voids all express and any implied warranties for the associated TI product or service and is an unfair and deceptive business practice. TI is not responsible or liable for any such statements.

Mailing Address:

Texas Instruments Post Office Box 655303 Dallas, Texas 75265

Copyright © 2002, Texas Instruments Incorporated