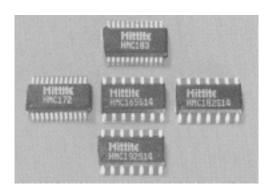


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GAAS MMICS FOR CHANGING BASE STATION REQUIREMENTS

oday wireless infrastructure designers are being faced with increasingly challenging requirements. Cellular base transceiver stations (BTS), or base station, are becoming smaller, smarter, higher performance, self-contained and lower cost simultaneously.

Early cellular BTS designs, which are still in use today, placed equipment in secured, environmentally controlled buildings at the base of an antenna tower. Engineers had to work with one or more closet-sized cabinets, tame environmental conditions, little limit on power consumption and moderate cost pressure. In contrast, handset designers have long been faced with severe size, weight, power and cost constraints.

Recent advances made in MMIC components to satisfy handset requirements are becoming ever more appropriate for the BTS engineer designing macro, micro and picocell equipment. BTS the size of a shoebox to a briefcase are not uncommon in current-generation equipment designs. Table 1 lists the differences between the old and new cellular BTS designs.

TABLE I

EVOLVING CELLULAR BASE STATION REQUIREMENTS

EVOLVINO CELEGEAR BASE STATION REGUIREMENTS								
Old Requirement	New Requirement							
analog analog and digital								
800/900 MHz	800/900 MHz and 1.8/1.9 GHz							
FDMA or TDMA	FDMA/TDMA/CDMA/							
	GSM/PDC							
macrocell	macro, mini, micro, pico							
omni or three sector	up to 12 sector,							
	dynamically configured							
indoor	indoor and outdoor							
small room at base	zoning restrictions on large							
of antenna tower	cell sites; wall, roof							
	or poletop mounting desired							
not limited,	somewhat limited,							
positive and negative	prefer positive only							
	Old Requirement analog analog and digital 800/900 MHz FDMA or TDMA macrocell omni or three sector indoor small room at base of antenna tower							

GaAs MMIC COMPONENTS FOR BTS

Innovative GaAs MMICs have been developed to meet these demanding and dynamic requirements. Monolithic, plastic-packaged devices including multithrow switches with integrated decoder drivers, single positive control voltage-variable attenuators (VVA), double-balanced mixers and frequency doublers enable BTS engineers to improve performance, reduce size and lower cost.

MINIATURE MULTITHROW MMIC SWITCHES FOR CELLULAR BTS

Multithrow switches are used in cellular BTS for receive - side antenna switching to one

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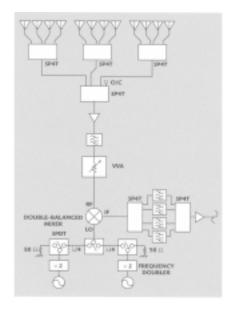
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TABLE II								
MMIC SWITCH SELECTION GUIDE								
Switches Type	Part Number	Frequency (GHz)	Insertion Loss/ Isolation (dB)	Control Lines/ Logic Type	Input IP3 (dBm)	Package Type	Actual Package Area (in²)	
SPDT	HMC190MS8	DC to 3	0.4/25	2, positive	+50	MSOP 8	0.022	
SPDT	HMC194MS8	DC to 3	0.7/50	2, positive	+43	MSOP 8	0.022	
SP4T	HMC165S14	DC to 2	0.5/32	2, negative	+42	SOIC 14	0.080	
SP4T	HMC18214	DC to 2	0.8/38	2, negative	+45	SOIC 14	0.080	
SP4T	HMC192S14	DC to 2	0.7/35	2, positive	+43	SOIC 14	0.080	
SP6T	HMC172QS24	DC to 2.5	0.6/27	3, negative	+40	QSOP 24	0.080	
SP8T	HMC183QS24	DC to 2	1.3/40	3, negative	+42	QSOP 24	0.080	



or more low noise amplifiers, to combine antenna paths on smart BTS systems for switched filter banks and switched delay lines, and to provide high isolation between differential LO sources. A new line of SPNT MMIC switches that operates from DC to 3 GHz, covering all BTS bands, has been developed. The product line comprises SPDT, SP4T, SP6T and SP8T switches, making it the most complete line of multithrow GaAs MMIC switches on the market today. These

switches include on-chip logic decoders and drivers that save components, board area and design time, and offer high third-order intercept (IP3) performance (+40 to +50 dBm). The switches are housed in standard plastic surface-mount technology (SMT) packages, space. In addition, the monolithic GaAS MMIC technology used provides consistency and high reliability.

Multithrow switches designs of the past used multiple PIN diodes or hybrid multithrow switched prior to the introduction of GaAs MMIC switches. To achieve an eight-throw configuration, up to 16 diodes and numerous control circuit components were required. Alternatively, cascaded multi-trow

hybrid switches could also perform the function. These approaches result in numerous control lines and components, reduced isolation due to control line cross talk and a relatively large complex board layout. A more contemporary SP8T approach uses one SPDT and two SP4T GaAS MMIC switches requiring 10 to 18 control lines and associated logic drive circuity (still not a small and simple approach). This article describes the alternate switching configurations utilized in

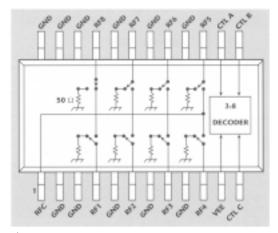
this new line of SPNT switches. Table 3 list important specifications of a sampling of the SPDT, SP4T, SP6T and SP8T products. All of the SPNT switches are fabricated using a standard commercial 1 μ m enhancement/depletion GaAs MESFET process. All of the switches have guaranteed specifications for operation from -40° to +85° C.

The model HMC192S14 SP4T switch is unique due to its positive voltage control and bias feature. The typical base station receiver diagram, shown in Figure 1, demonstrates how four HMC192S14 SP4Ts can be used in a 12element adaptive switching function at the receiver front end. A 12 sector antenna smart base station provides increased coverage and capacity over the traditional three sector system. Other SP4T products on the market require negative or positive /negative voltage supplies and up to eight control lines, and are housed in 24-lead wide body small outline ICs (SOIC) and 28-pin plastic leaded chip carrier packages. The smaller 14-lead SOIC size (0.080 sq in) incorporated in the SP4T version saves over 60 percent in PCB area vs. the more common (0.178 sq. in to 0.240 sq. in) packages.

The HMC183QS24 SP8T switch offers major benefits for adaptive switching functions in base stations, particularly saving in overall circuit size. The switch is the industry's first monolithic SP8T available in a low cost SMT package with an integrated 3:8 decoder driver. The SP8T switch provides a single-chip solution, reducing an equivalent SP8T discrete layout area consisting of two SP4Ts and one SPDT by over 90 percent. For the larger multithrow configurations shown in the typical base station receiver, the four HMC192S14 SP4Ts could be replaced by two HMC183QS24 SP8Ts and one HMC190MS8 SPDT to select between the SP8Ts. This configuration increases the available channels to 16, allowing for auxiliary or functional test inputs in parallel with the 12-element antenna receiver inputs. The 24-lead Quality Small Outline Package (QSOP) industry-standard plastic package occu-



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\$ 50.13 DECODER

▲ Fig. 3 The HMC192S14 SP4T switch

▲ Fig. 2 The HMC183QS24 SP8T switch

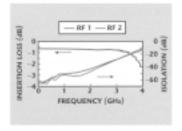
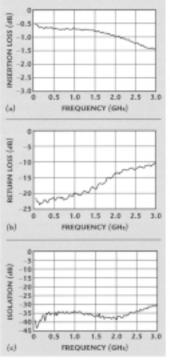


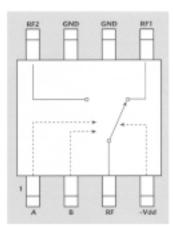
Fig. 5 The HMC194MS8 SPDT switch's Insertion loss and isolation



▲ Fig. 4 The HMC192S14 SP4T switch's (a) insertion loss, (b) return loss and (c) isolation

pies the same PCB are (0.080 sq. in) as each HMC192S14 SP4T 14-lead SOIC. The HMC183QS24 SP8T switch is shown in Figure 2.

The HMC192S14 device, shown in



 \triangle Fig. 6 The HMC194MS8 SPDT switch

Figure 3, requires only +5 V of bias at <5 mA and two positive - voltage CMOS-compatible control lines via an integrated 2:4 decoder. The RF1 to RF4 ports are nonreflective when in

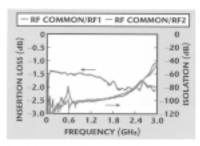
their off states. Figure 4 shows the SP4T's insertion loss, return loss and isolation. With only 0.7 to 1 dB insertion loss per switch, the total front-end matrix path loss through two switches (plus PCB and mismatch losses) is 1.7 to 2.4 dB at the 900 and 1900 MHz cellular bands, respectively. Isolation between paths is defined by the 35 to 37 dB single-switch channel-to-channel isolation. An input IP3 point of +43 dBm provides low distortion switching for technologies that demand a high dynamic range such as Code-Division Multiple Access (CDMA).

Another common BTS switch application is the selection of receive and transmit sections. This configuration can be accomplished using the new model HMC194MS8 high isolation SPDT switch. Less than 0.7 dB insertion loss is featured through 2.5 GHz. Isolation between channels is 50 and 42 dB at 1 and 2 GHz, respectively. Figure 5 shows the insertion loss and isolation for the ultra-small HMC194MS8 SPDT switch.

Housed in an industry-standard eight-lead mini small outline package (MSOP) (50 percent smaller than an eight-lead SOIC and 40 percent smaller than an eight-lead shrink small outline package (SSOP)), the HMC194MS8, shown in Figure 6, controlled by positive CMOS-compatible control volt-

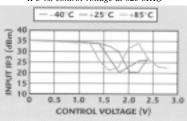


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▲ Fig. 7 The LO switch assembly's insertion loss and isolation

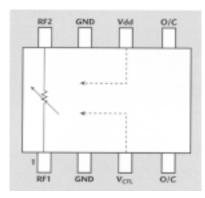
Fig. 8 The HMC173M38 VVA's input IP3 vs. control voltage at 825 MHz.



ages. The MSOP package occupies an area of 0.118" x 0.192" and a lead pith of 25 mil. Lead coplanarity is maintained to 3 mils. The RF1 and RF2 port are reflective open circuits when in their off states.

The typical base station diagram shows the configuration of three HMC194MS8 switches into a high isolation terminated SPDT. One-quarter wavelength transmission lines are used between the common switch and each outrigger switch to enhance the doubled HMC194MS8 isolation by another 10 to 15 dB. This high isolation switching structure was designed and fabricated in house to demonstrate the performance of the HMC194MS8 switch in this base station application. Over 90 dB isolation at -40° to +85° C was achieved from 700 to 2000 MHz with only three model HMC194MS8 switches. Figure 7 shows the performance of the high switch PCB assembly. Care was taken to decouple the six control lines and common V_{dd} bias switches.

A HIGH IP3 VVA



 \triangle Fig. 9 The HMC173M38 VVA

FOR CELLULAR BTS

For level control of the incoming signal in the typical BTS receiver, the new positive bias/control 800 to 2000 MHz HMC173MS8 VVA is offered. Figure 8 shows the VVA's input IP3 at -40°, +25° and +85° C, indicating in never falls below +20 dBm. Transmitter designers will find the HMC173MS8 VVA equally useful in the transmit power control loop just prior to the preamplifier. Previous MMIC VVA designs offered poor power handling (0 dBm or less input 1 dB compression point (P1dB) and poor linearity (+10 dBm or less IP3 at room temperature only).

Over 50 dB of attenuation range is available from 800 to 950 MHz and +10 dBm (min) over temperature, which is the best available power handling in the industry for GaAs MMIC VVAs. Housed in an industry standard eight-lead MSOP package, the VVA is 50 percent smaller (0.022 sq. in.) than an eight-lead SOIC and 40 percent smaller than an eight-lead SSOP, which house other typical VVAs. Figure 9 shows the functional diagram of the HMC173MS8 VVA.

CONCLUSION

Cellular BTS suppliers are working to meet the demands of cellular service providers and society in general to produce less obtrusive, aesthetically pleasing cellular sires and equipment. This new equipment must increase cellular coverage and subscriber capacity while improving overall communications quality. With these requirements in mind, cellular BTS engineers are demanding more performance, lower cost and smaller size from MMIC components. This new family of GaAs MMIC products can help BTS engineers meet their design objectives.

SPDT to SP8T monolithic switches with integrated drivers can help to improve and reduce the size of antenna, attenuator, filter and synthesizer matrices. The HMC173MS8 50 dB VVA with +21 dBm IP3 can help new systems meet their high dynamic range requirements. To augment these products, HMC175MS8 MMIC mixers in standard plastic packages offer high LO suppression, which is essential to reducing overall spurious levels in the RF/IF bands, and HMC187MS8 passive frequency doublers do not contribute phase noise while isolating the fundamental input by over 45 dB.

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